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(71) Applicant: **TEXACO CHEMICAL COMPANY**
3040 Post Oak Boulevard
Houston, Texas 77056(US)

(72) Inventor: **Primeaux II, Dudley Joseph**
Route 4, Box 229-B4
Elgin, Texas 78621(US)

(74) Representative: **Brock, Peter William et al**
URQUHART-DYKES & LORD 91 Wimpole
Street
London W1M 8AH(GB)

(84) **Spray polyurea elastomers with improved abrasion resistance.**

(57) Spray polyurea elastomers comprising an (A) component which includes an isocyanate, and a (B) component which includes (1) an amine terminated polyoxyalkylene polyol and (2) a chain extender, can be made resistant to abrasion by the inclusion of a chemically sized filler material. Suitable filler materials are calcium metasilicate, milled glass, flaked glass, mica or glass spheres; which may be chemically sized by treatment with, for example epoxy silanes, amino silanes or titanate or zirconate coupling agents.

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SPRAY POLYUREA ELASTOMERS WITH IMPROVED ABRASION RESISTANCE

The present invention relates generally to spray polyurea elastomers and, more specifically, to spray polyurea elastomers which include chemically sized mineral particles, thereby improving the abrasion resistance of the cured elastomer.

Elastomer systems are commonly recognized as, among other things, coating materials, with spray polyurea elastomer systems being particularly useful when employed in this capacity. One of the considerations confronting the skilled artisan is the abrasion resistance of the coating after it is ultimately applied to a substrate. In accordance with the present invention the abrasion resistance of a spray polyurea elastomer is improved by incorporating chemically sized mineral particles in the system as is discussed with particularity hereinbelow.

U.S. Patent No. 4,585,850 describes a reaction injection molded (RIM) elastomer made by reacting, in a closed mold, an amine terminated polyether of greater than 1500 average molecular weight, having greater than 50% of their active hydrogens in the form of amine hydrogens; a chain extender; flaked glass pretreated with an amino silane coupling agent; and an aromatic polyisocyanates. The '850 patent referred to above contains a discussion of other applications and patents in the field; for example, U.S. Patent Nos. 4,474,900 and 4,507,090, and is incorporated herein by reference. Similarly, U.S. Patent No. 4,716,193 describes a reactive glass component employed in a reinforced reaction injection molded elastomer. However, since these patents relate to RIM elastomers, patentees are not concerned with abrasion resistance. Specifically, RIM articles are invariably formed in a closed mold and, accordingly, the elastomeric material used to form the molded article becomes pressurized within the mold as additional amounts of elastomer are introduced therein. As a result, the density of the thus formed article is greater at the locus of the surface or skin, relative to the density at the locus of the core. The increased surface density of a RIM article provides a characteristic resistance to abrasion. This phenomenon is not exhibited by spray polyurea coatings, inasmuch as the coating is sprayed onto a substrate, i.e., an open mold, and, accordingly, the pressure required to provide the increased surface density is unavailable.

Furthermore, since the article formed via RIM typically has a topcoat, the degree to which the RIM article exhibits resistance to abrasion is even further enhanced.

U.S. Patent No. 3,979,364 describes the use of aminated polyethers as hereinafter used as a component with a polyol to make an elastomer. U.S. Patent No. 3,666,788 describes the use of cyanoalkylated aminated polyethers in spray systems. The '788 disclosure, in Column 1, states that the aminated polyethers as used hereinafter cannot be used in spray coatings due to very rapid reaction rates with isocyanates.

U.S. Patent Nos. 4,379,729; 4,444,910 and 4,433,067 describe elastomers which are prepared using a high molecular weight amine terminated polyether, an aromatic diamine chain extender and an aromatic polyisocyanate which may merely be a polyisocyanate or a quasi-prepolymer prepared from a polyol reacted with a polyisocyanate wherein some isocyanate groups are still left unreacted. Various patents have been applied for and received using the basic combination recited above as well as various mold release agents and other additives, such as catalysts and fillers, including glass fibers. For example, see U.S. Patent No. 4,607,090.

Polyoxyalkylene polyamines, particularly JEFFAMINE® T-403, D-400 and D-230, are described as chain extenders in U.S. Patent No. 4,732,919; however, this patent relates to an elastomer system to be used in a RIM application.

The publication "Silane Effects and Machine Processing in reinforced High Modulus RIM urethane Composites," by E.G. Schwartz, et al., Journal of Elastomers and Plastics, vol. 11 (Oct. 1979), page 280, describes the use of silane treated milled glass fibers in reinforced RIM composites.

The publication "Surface Modification for RRIM Urethanes," by Ed Galli, Plastics Compounding - (Jan/Feb 1982) describes silane treated glass fiber reinforcement of RRIM urethanes.

Commonly assigned U.S. Patent Application Serial No. 261,193 describes spray polyurea elastomers which include roved filler materials that are externally added. A method for making those elastomers is also described.

Therefore, it is my understanding that a spray polyurea elastomer system which includes chemically sized filler materials incorporated directly in the elastomer and which exhibits favorable resistance to abrasion, especially when employed as a coating, has heretofore been unavailable.

SUMMARY OF INVENTION

Accordingly, the present invention relates to a spray polyurea elastomer which comprises an (A) component and a (B) component. The (A) component includes an isocyanate. Preferably, the isocyanate of component (A) includes a quasi-prepolymer of an isocyanate and a material selected from at least one polyol, a high molecular weight polyoxyalkyleneamine or a combination of these materials. The (B) component includes (1) an amine terminated polyoxyalkylene polyol, (2) a chain extender and (3) a chemically sized filler material employed in an amount sufficient to make the elastomer substantially resistant to abrasion.

The present invention also relates to a method for making a spray polyurea elastomer coating which is substantially resistant to abrasion. Specifically, the method of this invention comprises directing a first and second reactive stream into mutual contact with each other to effectuate a mixing of the first and second reactive streams. The first reactive stream includes an isocyanate and the second reactive stream includes an amine terminated polyoxyalkylene polyol, a chain extender and a chemically sized filler material. The mixed first and second reactive streams are delivered onto a substrate in a manner such that the substrate becomes coated with the mixed first and second reactive streams. The mixture of the first and second reactive streams is then permitted to cure on the substrate to form the spray polyurea elastomer coating. The chemically sized filler material is employed in the elastomer in an amount sufficient to make the elastomer coating substantially resistant to abrasion.

Advantageously, in addition to exhibiting substantial resistance to abrasion, the polyurea spray elastomer of the present invention exhibits other favorable characteristics, such as good thermal stability, tear resistance and flexural modulus. Also, the processing characteristics of the elastomer, such as speed and flexibility, are improved.

Generally, the present method involves spraying onto a substrate; specific substrates include, but are not limited to, open molds to manufacture, among other things, bathtubs, shower stalls, automotive parts, boat hulls and in other applications where fiberglass resins, epoxies and polyesters are typically being used.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

The isocyanates employed in component (A) are those known to one skilled in the art. Thus, for instance, they can include aliphatic isocyanates of the type described in U.S. Patent No. 4,748,192. Accordingly, they are typically aliphatic diisocyanates, and, more particularly, are the trimerized or the biuretic form of an aliphatic diisocyanate, such as hexamethylene diisocyanate, or the bifunctional monomer of the tetraalkyl xylene diisocyanate, such as the tetramethyl xylene diisocyanate. Cyclohexane diisocyanate is also to be considered a preferred aliphatic isocyanate. Other useful aliphatic polyisocyanates are described in U.S. Patent No. 4,705,814. They include aliphatic diisocyanates, for example, alkylene diisocyanates with 4 to 12 carbon atoms in the alkylene radical, such as 1,12-dodecane diisocyanate and 1,4-tetramethylene diisocyanate. Also described are cycloaliphatic diisocyanates, such as 1,3 and 1,4-cyclohexane diisocyanate as well as any desired mixture of these isomers, 1-isocyanato-3,3,5-trimethyl-5-isocyanatomethyl-cyclohexane (isophorone diisocyanate); 4,4',2,2'- and 2,4'-dicyclohexylmethane diisocyanate as well as the corresponding isomer mixtures, and the like.

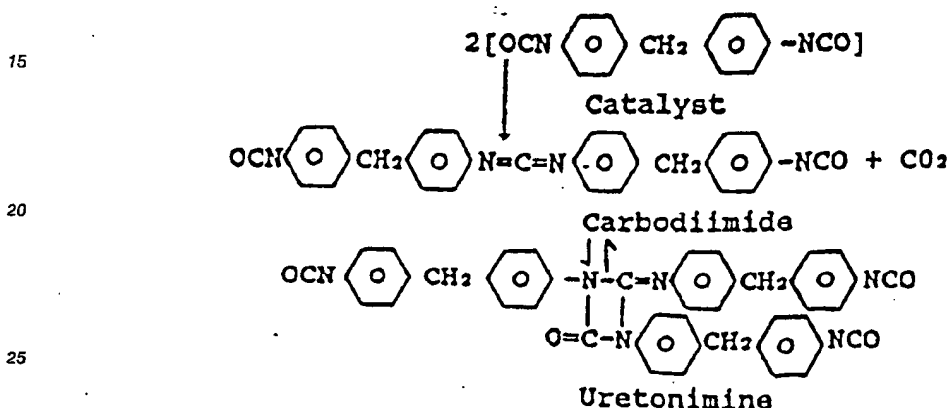
A wide variety of aromatic polyisocyanates may be used to form the elastomer of the present invention. Typical aromatic polyisocyanates include p-phenylene diisocyanate, polymethylene polyphenylisocyanate, 2,6-toluene diisocyanate, dianisidine diisocyanate, bitolylene diisocyanate, naphthalene-1,4-diisocyanate, bis(4-isocyanatophenyl)methane, bis(3-methyl-3-isocyanatophenyl)methane, bis(3-methyl-4-isocyanatophenyl)methane, and 4,4'-diphenylpropane diisocyanate.

Other aromatic polyisocyanates used in the practice of the invention are methylene-bridged polyphenyl polyisocyanate mixtures which have a functionality of from about 2 to about 4. These latter isocyanate compounds are generally produced by the phosgenation of corresponding methylene bridged polyphenyl polyamines, which are conventionally produced by the reaction of formaldehyde and primary aromatic amines, such as aniline, in the presence of hydrochloric acid and/or other acidic catalysts. Known processes for preparing polyamines and corresponding methylene-bridged polyphenyl polyisocyanates therefrom are described in the literature and in many patents, for example, U.S. Patent Nos. 2,683,730; 2,950,263; 3,012,008; 3,344,162 and 3,362,979.

Usually methylene-bridged polyphenyl polyisocyanate mixtures contain about 20 to about 100 weight percent methylene diphenyldiisocyanate isomers, with the remainder being polymethylene polyphenyl diisocyanates having higher functionalities and higher molecular weights. Typical of these are polyphenyl polyisocyanate mixtures containing about 20 to 100 weight percent diphenyldiisocyanate isomers, of which

20 to about 95 weight percent thereof is the 4,4'-isomer with the remainder being polymethylene polyphenyl polyisocyanates of higher molecular weight and functionality that have an average functionality of from about 2.1 to about 3.5. These isocyanate mixtures are known, commercially available materials and can be prepared by the process described in U.S. Patent No. 3,362,979.

5 By far the most preferred aromatic polyisocyanate is methylene bis(4-phenylisocyanate) or MDI. Pure MDI, quasi-prepolymers of MDI, modified pure MDI, etc. are useful. Materials of this type may be used to prepare suitable RIM elastomers. Since pure MDI is a solid and, thus, often inconvenient to use, liquid products based on MDI or methylene bis(4-phenylisocyanate) are used herein. U.S. Patent No. 3,394,164 describes a liquid MDI product. More generally, uretonimine modified pure MDI is included also. This
10 product is made by heating pure distilled MDI in the presence of a catalyst. The liquid product is a mixture of pure MDI and modified MDI and is represented as follows:



30 Examples of commercial materials of this type are Dow's ISONATE® 125M (pure MDI) and ISONATE 143L ("liquid" MDI). Preferably the amount of isocyanates used is the stoichiometric amount based on all the ingredients in the formulation or greater than the stoichiometric amount.

Of course, the term isocyanate also includes quasi-prepolymers of isocyanates or polyisocyanates with active hydrogen containing materials. The active hydrogen containing materials can include, but are not limited to, a polyol or polyols, a high molecular weight polyoxyalkyleneamine or combinations thereof.

35 The polyols include polyether polyols, polyester diols, triols, tetrols, etc., having an equivalent weight of at least about 500, and preferably at least about 1,000 up to about 3,000. Those polyether polyols based on trihydric initiators of about 4,000 molecular weight and above are especially preferred. The polyethers may be prepared from ethylene oxide, propylene oxide, butylene oxide or mixtures of propylene oxide, butylene oxide and/or ethylene oxide. Other high molecular weight polyols which may be useful in this invention are
40 polyesters of hydroxyl terminated rubbers, e.g., hydroxyl terminated polybutadiene. Hydroxyl terminated quasi-prepolymers of polyols and isocyanates are also useful in this invention.

Especially preferred are amine terminated polyether polyols, including primary and secondary amine terminated polyether polyols of greater than 1,500 average molecular weight having from about 2 to about 6 functionality, preferably from about 2 to about 3, and an amine equivalent weight of from about 750 to about
45 4,000. Mixtures of amine terminated polyethers may be used. In a preferred embodiment the amine terminated polyethers have an average molecular weight of at least about 2,500. These materials may be made by various methods known in the art.

The amine terminated polyether resins useful in this invention, for example, are polyether resins made from an appropriate initiator to which lower alkylene oxides, such as ethylene oxide, propylene oxide,
50 butylene oxide or mixtures thereof, are added with the resulting hydroxyl terminated polyol then being aminated.

When two or more oxides are used, they may be present as random mixtures or as blocks of one or the other polyether. In the amination step it is highly desirable that the terminal hydroxyl groups in the polyol be essentially all secondary hydroxyl groups for ease of amination. Normally, the amination step
55 does not completely replace all of the hydroxyl groups. However, the majority of hydroxyl groups are replaced by amine groups. Therefore, in a preferred embodiment, the amine terminated polyether resins useful in this invention have greater than 50 percent of their active hydrogens in the form of amine hydrogens. If ethylene oxide is used it is desirable to cap the hydroxyl terminated polyol with a small

amount of higher alkylene oxide to ensure that the terminal hydroxyl groups are essentially all secondary hydroxyl groups. The polyols so prepared are then reductively aminated by known techniques, for example, as described in U.S. Patent No. 3,654,370, the contents of which is incorporated herein by reference.

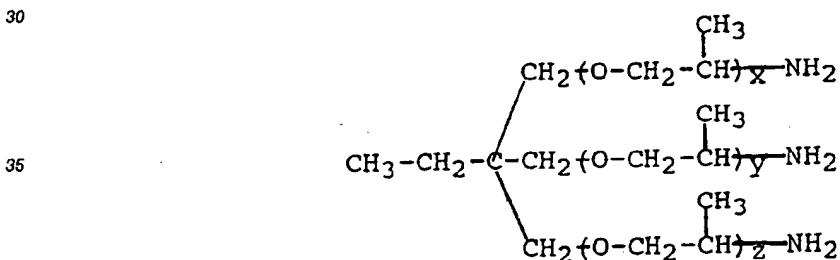
In the practice of this invention, a single high molecular weight amine terminated polyol may be used.
 5 Also, mixtures of high molecular weight amine terminated polyols, such as mixtures of di- and trifunctional materials and/or different molecular weight or different chemical composition materials, may be used.

Also, high molecular weight amine terminated polyethers or simply polyether amines are included within the scope of my invention and may be used alone or in combination with the aforesaid polyols. The term high molecular weight is intended to include polyether amines having a molecular weight of at least about
 10 2000. Particularly preferred are the JEFFAMINE® series of polyether amines available from Texaco Chemical Company; they include JEFFAMINE D-2000, JEFFAMINE D-4000, JEFFAMINE T-3000 and JEFFAMINE T-5000. These polyether amines are described with particularity in Texaco Chemical Company's product brochure entitled THE JEFFAMINE POLYOXYALKYLENEAMINES.

The (B) component of the present spray polyurea elastomer system includes an amine terminated
 15 polyoxyalkylene polyol and a chain extender. The amine terminated polyoxyalkylene polyol is preferably selected from diols or triols and, most preferably, includes a blend of diols and/or triols. The particular polyols, i.e., diols and/or triols, employed in component (B) are the same as those described hereinabove in connection with the quasi-prepolymer of component (A).

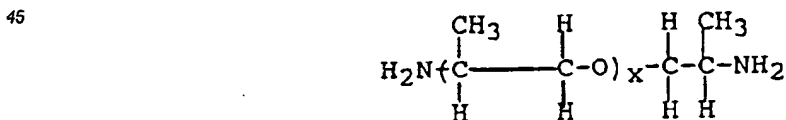
The chain extenders useful in this invention include, for example, 1-methyl-3,5-diethyl-2,4-diaminobenzene,
 20 1-methyl-3,5-diethyl-2,6-diaminobenzene (both of these materials are also called diethyltoluene diamine or DETDA), 1,3,5-triethyl-2,6-diaminobenzene, 3,5,3',5'-tetraethyl-4,4'-diaminodiphenylmethane and the like. Particularly preferred aromatic diamine chain extenders are 1-methyl-3,5-diethyl-2,4-diaminobenzene or a mixture of this compound with 1-methyl-3,5-diethyl-2,6-diaminobenzene. It is within the scope of this invention to include some aliphatic chain extender materials as described in U.S. Patent Nos. 4,246,363
 25 and 4,269,945.

Other chain extenders included amine terminated chain extenders which are generally described as low molecular weight polyoxyalkylene polyamines containing terminal amine groups. One particular chain extender is represented by the formula:



wherein $x+y+z$ has a value of about 5.3. The average amine hydrogen equivalent weight is about 67 and the product is commercially available from Texaco Chemical Company as JEFFAMINE T-403.

Another related polyoxypropylene chain extender is represented by the formula:



wherein x has a value of about 5.6. This product has an average amine hydrogen equivalent weight of about 100 and is commercially available from Texaco Chemical Company as JEFFAMINE D-400. The product having the same formula as above wherein x has an average value of about 2.6 is useful. This product has an average amine hydrogen equivalent weight of about 57.5 and is commercially available from Texaco
 55 Chemical Company as JEFFAMINE D-230.

Other chain extenders will be apparent to those skilled in the art and the above recitation is not intended to be a limitation on the invention claimed herein.

The chemically sized filler materials can be employed in component (A) or (B), preferably they are

employed in component (B). These materials are preferably mineral particles, such as calcium metasilicate, milled glass, flaked glass, mica and glass spheres, which have been chemically sized by being subjected to treatment with a sizing agent, such as amino silanes and epoxy silanes. The sizing agent can also be selected from amine terminated titanate and zirconate coupling agents, which are available from Kenrich Petrochemicals Inc., Bayonne, N.J. The sizing agent functions to provide a chemical bond between the spray polyurea elastomer and the filler materials. One particularly preferred mineral particle is WOLLASTOKUP® 10012, an amino silane treated Wollastonite, available from NYCO, a division of Canadian Pacific (U.S.) Inc.

The chemically sized filler particles are generally employed in an amount of up to 25 weight percent of the overall elastomer. Preferably, the filler particles are employed in an amount of about 5 to about 20 weight percent.

Since the present invention relates to a spray polyurea elastomer, the particle size of the filler is a significant aspect. Generally, the filler materials must be small enough so that they are permitted to pass through the orifice of the spray apparatus. Therefore, filler particles used in RIM applications are typically not well suited for use in the instant invention. The size of the filler particles used herein can range from about 1/256 inch to about 1/32 inch, with the preferred size ranging from about 1/128 inch to about 1/64 inch.

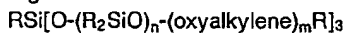
Optionally, the present spray polyurea elastomer can include an internal mold release agent to facilitate the removal of the cured elastomer from the open mold. While the release agent, if employed, can be incorporated into the (A) or (B) component, it is preferably incorporated in the (B) component. The internal mold release agents useful in the present invention are known to those skilled in the art; they include, but are not limited to, zinc stearate, sodium oleate and silicone agents.

Advantageously, the (A) and (B) components react to form the present elastomer system without the aid of a catalyst. However, if desired, a catalyst can be used.

Catalysts such as tertiary amines or an organic tin compound may suitably be a stannous or stannic compound, such as a stannous salt of a carboxylic acid, a trialkyltin oxide, a dialkyltin dihalide, a dialkyltin oxide, etc., wherein the organic groups of the organic portion of the tin compound are hydrocarbon groups containing from 1 to 8 carbon atoms. For example, dibutyltin dilaurate, dibutyltin diacetate, diethyltin diacetate, dihexyltin diacetate, di-2-ethylhexyltin oxide, dioctyltin dioxide, stannous octoate, stannous oleate, etc., or a mixture thereof, may be used.

Tertiary amine catalysts include trialkylamines (e.g., trimethylamine, triethylamine); heterocyclic amines, such as N-alkylmorpholines (e.g., N-methylmorpholine, N-ethylmorpholine, dimethyldiaminodiethylether, etc.), 1,4-dimethylpiperazine, triethylenediamine, etc.; and aliphatic polyamines, such as N,N,N',N'-tetramethyl-1,3-butanediamine.

Other conventional formulation ingredients may be employed in component (A) or (B) as needed, such as, for example, foam stabilizers, also known as silicone oils or emulsifiers. The foam stabilizers may be an organic silane or siloxane. For example, compounds may be used having the formula:



wherein R is an alkyl group containing from 1 to 4 carbon atoms; n is an integer of from 4 to 8; m is an integer of from 20 to 40; and the oxyalkylene groups are derived from propylene oxide and ethylene oxide. See, for example, U.S. Patent No. 3,194,773.

Pigments, for example titanium dioxide, may be incorporated in the elastomer system, preferably in the (B) component, to impart color properties to the elastomer.

Post curing of the elastomer of the invention is optional. Post curing will improve some elastomeric properties, such as heat sag. Employment of post curing depends on the desired properties of the end product.

The (A) component and (B) component of the present spray polyurea elastomer system are combined or mixed under high pressure; most preferably, they are impingement mixed directly in the high pressure spray equipment, which is, for example, a GUSMER® H-V proportioner fitted with a GUSMER Model GX-7 spray gun. In particular, a first and second pressurized stream of components (A) and (B), respectively, are delivered from two separate chambers of the proportioner and are impacted or impinged upon each other at high velocity to effectuate an intimate mixing of the two components and, thus, the formation of the elastomer system, which is then coated onto the desired substrate via the spray gun.

In a preferred embodiment, the mixing module of the GUSMER GX-7 spray gun is modified by installing carbide mixing chambers to avoid the potential for the deterioration of the plastic chamber by the sized filler particles.

The volumetric ratio of the (A) component to the (B) component is generally from about 30 to 70 percent to about 70 to 30 percent. Preferably, component (A) and component (B) are employed in a 1:1

volumetric ratio.

GLOSSARY OF TERMS AND MATERIALS

- 5
 TEXOX® PPG-2000 - Polypropylene oxide of about 2000 molecular weight; a product of Texaco Chemical Company.
 ISONATE® 143 L - Carbodiimide modified liquid MDI; a product of the Upjohn Company.
 THANOL® SF-5505 - A 5500 molecular weight polyether triol containing approximately 80% primary
 10 hydroxide groups.
 FOMREZ® EPD-28 - Polypropylene oxide block, ethylene oxide capped polyol of about 4000 molecular weight; a product of WITCO Corp.
 JEFFAMINE® T-5000 - Polypropylene oxide triamine of about 5000 molecular weight; a product of Texaco Chemical Company.
 15 JEFFAMINE® T-3000 - Polypropylene oxide triamine of about 3000 molecular weight; a product of Texaco Chemical Company.
 JEFFAMINE® D-4000 - Polypropylene oxide diamine of about 4000 molecular weight; a product of Texaco Chemical Company.
 JEFFAMINE® D-2000 - Polypropylene oxide diamine of about 2000 molecular weight; a product of Texaco
 20 Chemical Company.
 JEFFAMINE® T-403, D-400 and D-230 are described with particularity hereinabove.

The following examples are provided to further illustrate preferred embodiments of the present invention and should not be construed as limiting the present invention in any way.

- In the examples, all spray work was performed with a GUSMER H-V high pressure proportioner with a
 25 model GX-7 spray gun. The elastomer systems were sprayed using a block temperature of 160° F on the (A) component side and 150° F on the (B) component side, with a hose temperature of 160° F. The system output ranged from 17.5 lbs/min to 22.5 lbs/min with a line pressure ranging from 2500 to 3000 psig on the (A) component side and 2000 to 2500 psig on the (B) component side. Each of the elastomer systems produced in the examples were mixed at an (A) : (B) volumetric ratio of 1:1. The (B) component containing
 30 the filler material did not require agitation as it would have in RIM mixing equipment.

EXAMPLE I

- 35 The (A) component of a spray polyurea elastomer was prepared by combining 60 parts of ISONATE 143L and 40 parts of THANOL SF-5505 to form a quasi-prepolymer. The (B) component was prepared by combining 27.07 parts of JEFFAMINE T-5000, 18.05 parts of JEFFAMINE D-4000, 12.41 parts of JEFFAMINE D-2000, 32.15 parts of DETDA and 10.32 parts of WOLLASTOKUP 10012. The (A) and (B)
 40 components were mixed in the high pressure spray equipment at an (A) : (B) weight ratio of 1.066. The resulting reinforced polymer elastomer was sprayed onto a flat metal substrate coated with a zinc stearate based external mold release agent and exhibited a gel time of 1.8 seconds. As spraying proceeded, a change in the systems pressure was noted, which was ascribed to the deterioration of the mixing orifices on the (B) component side of the plastic mixing module by the sized mineral particles.

COMPARATIVE EXAMPLE I(A)

- 45 The (A) component of the spray polyurea elastomer produced in this example was prepared in accordance with Example I. The (B) component was prepared by combining 31.2 parts of JEFFAMINE T-5000, 20.8 parts of JEFFAMINE D-4000, 14.3 parts of JEFFAMINE D-2000 AND 33.7 parts of DETDA. The
 50 (A) and (B) components were mixed in the high pressure spray equipment at an (A):(B) weight ratio of 1.131. The polyurea elastomer produced in this example was sprayed in accordance with Example I.

The physical properties of the polyurea elastomers produced in Example I and Comparative Example I-(A) were analyzed; the results are reported in Table I.

55

TABLE I

	Example I	Comparative Example I(A)
% glass	4.61	0
Tensile (psi)	2058	2522
Elongation (%)	30	123
Tear (pli)	516	504
Shore D hardness (0 sec)	57	62
(10 sec)	52	58
Flexural modulus (psi)		
77° F	70705	48118
158° F	42942	42171
-20° F	115088	110973
Impact, notched (ft.lbs/in)	3.44	9.15
Heat sag (mm)		
100 mm - 250° F/60 min	0	3.0
150 mm - 250° F/60 min	4.0	15.0
100 mm - 311° F/60 min	4.0	-
150 mm - 311° F/60 min	18.5	-
Abrasion resistance (1000 gm, 1000 rev, H-18 wheels wt loss in mg)	280	550

As these data demonstrate, the spray polyurea elastomer of the present invention, which includes the chemically sized filler materials (Example I), exhibits an abrasion resistance that is nearly 100% better than an elastomer that is devoid of the chemically sized particles (Comparative Example I(A)). These data further establish other improved properties of the elastomer of Example I relative to those exhibited by the elastomer of Comparative Example I(A), such properties include tear resistance, flexural modulus and high temperature properties.

EXAMPLE II

The (A) component of a spray polyurea elastomer was prepared by combining 50 parts of ISONATE 143L and 50 parts of FOMREZ EPD-28. The (B) component was prepared by combining 39.7 parts of JEFFAMINE T-5000, 24.8 parts of JEFFAMINE D-2000, 23.8 parts of DETDA, 1.5 parts of zinc stearate and 10.2 parts of WOLLASTOKUP 10012. The (A) and (B) components were mixed in the high pressure spray equipment at an (A):(B) weight ratio of 1.031. The resulting reinforced polyurea elastomer was sprayed onto a flat metal substrate with no external mold release agent and exhibited a gel time of 2.0 seconds. The spray gun was modified to include carbide internal mixing components and, as a result, no pressure deviation was experienced.

COMPARATIVE EXAMPLE II (a)

The (A) component of the spray polyurea elastomer produced in this Example was prepared in accordance with Example II. The (B) component was prepared by combining 45.0 parts of JEFFAMINE T-5000, 28.2 parts of JEFFAMINE D-2000, 25.3 parts of DETDA and 1.5 parts of zinc stearate. The (A) and (B) components were mixed in the high pressure spray equipment at an (A):(B) weight ratio of 1.107. The resulting polyurea elastomer was sprayed onto the flat metal substrate as in Example II.

The physical properties of the polyurea elastomer produced Example II and Comparative Example II(A) were analyzed; the results are reported in Table II.

TABLE II

	Example 2	Comparative Example No. II(A)
% glass	4.76	0
Tensile (psi)	1895	1741
Elongation (%)	247	267
Tear (pli)	408	344
Flexural modulus (psi)		
77 ° F	26583	19581
158 ° F	17912	13509
-20 ° F	57273	44671
Impact, notched (ft.lbs/in)	7.42	4.24
Heat sag (mm)		
100 mm - 250 ° F/60 min	3.0	4.0
150 mm - 250 ° F/60 min	17.5	28.0
Abrasion resistance (1000 gm, 1000 rev, H-18 wheels wt loss in mg)	290	520

As these data demonstrate, the spray polyurea elastomer of the present invention, which includes the chemically sized filler materials (Example II), exhibits an abrasion resistance that is nearly 90% better than an elastomer that is devoid of the chemically sized particles (Comparative Example II(A)). These data further establish other improved properties of the present elastomer, such as tear resistance, flexural modulus and high temperature properties.

Claims

1. A spray polyurea elastomer comprising an (A) component which includes an isocyanate, and a (B) component which includes (1) an amine terminated polyoxyalkylene polyol and (2) a chain extender, characterized in that the elastomer contains a chemically sized filler material in an amount sufficient to make said elastomer substantially resistant to abrasion.
2. An elastomer according to Claim 1 characterized in that the chemically sized filler material is calcium metasilicate, milled glass, flaked glass, mica or glass spheres.
3. An elastomer according to Claim 1 or 2 characterized in that the filler material is chemically sized by treatment with a sizing agent selected from epoxy silanes, amino silanes and titanate or zirconate coupling agents.
4. An elastomer according to any one of Claims 1 to 3 characterized in that the filler material is employed in an amount of 5 to 20 weight percent.
5. An elastomer according to any one of Claims 1 to 4 characterized in that the filler material has a size from 0.198 to 0.397 mm.
6. An elastomer according to any one of Claim 1 to 5 characterized in that the component (a) comprises a quasi-prepolymer of said isocyanate and a material selected from at least one polyol, a high molecular weight polyoxyalkyleneamine or combination of said materials.
7. An elastomer according to Claim 6 characterized in that the polyol of said quasi-prepolymer and said amine terminated polyoxyalkylene polyol of component (B) comprise polyether polyols or polyester polyols having an equivalent weight of at least 500.
8. An elastomer according to Claim 6 characterized in that the polyester polyols are polyesters of hydroxyl terminated rubbers.
9. An elastomer according to Claim 6 characterized in that polyether polyols are selected from polyols based on trihydric initiators having a molecular weight of at least 4000; amine terminated polyether polyols having an average molecular weight greater than 1500, a functionality of 2 to 6 and an amine equivalent weight of 750 to 4000; and mixtures thereof.
10. An elastomer according to Claim 6 characterized in that the polyether polyols are derived from amine terminated polyether resins having greater than 50 percent of their active hydrogens in the form of amine

hydrogens.

11. An elastomer according to any one of Claims 1 to 10 characterized in that the chain extender is 1-methyl-3,5-diethyl-2,4-diaminobenzene; 1-methyl-2,5-diethyl-2,6-diaminobenzene; a mixture of 1-methyl-3,5-diethyl-2,4-diaminobenzene and 1-methyl-3,5-diethyl-2,6-diaminobenzene; 1,3,5-triethyl-2,6-diaminobenzene; 3,5,3',5'-tetraethyl-4,4'-diaminodiphenylmethane; or a polyoxyalkylene polyamine having terminal amine groups.

12. A method for making an abrasion-resistant spray polyurea elastomer coating according to any one of Claims 1 to 11 comprising (a) directing a first reactive stream of the (A) component and a second reactive stream of the (B) component into mutual contact to form a mixture, (b) delivering said mixture onto a substrate in a manner such that said substrate becomes coated with said mixture and (c) permitting said mixture to cure on said substrate to form said spray polyurea elastomer coating, characterized in that said chemically sized filler material is incorporated in said (A) component and/or said (B) component.

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EUROPEAN SEARCH REPORT

Application Number

EP 90 30 9632

DOCUMENTS CONSIDERED TO BE RELEVANT					
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)		
D,Y	US-A-4 585 850 (R.J.G. DOMINGUEZ) * Claims 1-3; column 2, line 47 - column 3, line 68; column 6, lines 3-6 * - - - -	1-4,6-12	C 08 K 9/04 C 08 G 18/10 C 08 G 18/66 C 08 G 18/50		
P,Y	EP-A-0 366 297 (TEXACO)(02-05-1990) * Claims 1-8; page 4, line 46 - page 5, line 10 * - - - -	1-4,6-12			
D,A	US-A-4 474 900 (R.J.G. DOMINGUEZ) * Claims 1-7,10; column 5, line 60 - column 6, line 32 * - - - -	1			
A	EP-A-0 287 192 (TEXACO) * Claims 1,4; page 5, lines 44-56 * - - - -	1			
A	US-A-4 695 618 (N.R. MOWRER) * Claims 1-5; column 6, lines 22-31 * - - - - -	1			
The present search report has been drawn up for all claims			TECHNICAL FIELDS SEARCHED (Int. Cl.5) C 08 G C 08 K		
Place of search The Hague		Date of completion of search 11 March 91	Examiner VAN PUymbroeck M.A.		
<table><tr><td>CATEGORY OF CITED DOCUMENTS X: particularly relevant if taken alone Y: particularly relevant if combined with another document of the same category A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention</td><td>E: earlier patent document, but published on, or after the filing date D: document cited in the application L: document cited for other reasons &: member of the same patent family, corresponding document</td></tr></table>				CATEGORY OF CITED DOCUMENTS X: particularly relevant if taken alone Y: particularly relevant if combined with another document of the same category A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention	E: earlier patent document, but published on, or after the filing date D: document cited in the application L: document cited for other reasons &: member of the same patent family, corresponding document
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